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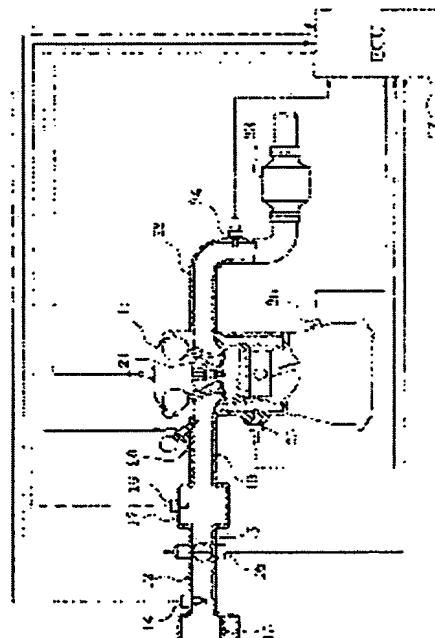
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## (54) ABNORMALITY DIAGNOSIS DEVICE OF INTERNAL COMBUSTION ENGINE

### (57)Abstract:

**PROBLEM TO BE SOLVED:** To prevent such an erroneous diagnosis that a disturbance of an output of an exhaust gas sensor occurring due to dispersion among cylinders of an engine is determined to be an abnormality of the exhaust gas sensor.

**SOLUTION:** A dispersion value among the cylinders is calculated for each of the cylinders based on behavior of such as an intake pipe pressure detected by an intake pipe pressure sensor 18, and a fuel injection amount and the like is corrected for each of the cylinders based on the dispersion value between the cylinders thereby correcting the dispersion among the cylinders. When the dispersion value between the cylinders exceeds a predetermined value during engine operating, or until correction of the dispersion among the cylinders is completed, it is determined that the disturbance of the output of the exhaust gas sensor 24 occurring due to the dispersion between cylinders is likely to exceed a normal range, thereby prohibiting the abnormality diagnosis of the exhaust gas sensor 24 or alleviating an abnormal determination reference. Accordingly, the erroneous diagnosis such that the disturbance of the output of the exhaust gas sensor occurring due to the dispersion among the cylinders is determined to be abnormality of the exhaust gas sensor is prevented.



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**CLAIMS**

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[Claim(s)]

[Claim 1]

In the abnormality diagnostic equipment of the internal combustion engine having an abnormality diagnostic means to perform a predetermined abnormality diagnosis based on the output of the sensor which detects the information about the operational status of the internal combustion engine which has two or more gas columns,

A dispersion detection means between gas columns to calculate the dispersion value between gas columns showing dispersion in the operational status between said internal combustion engine's gas columns,

An incorrect diagnostic prevention means to perform prohibition of the abnormality diagnosis by said abnormality diagnostic means, or relaxation of an abnormality criterion when said dispersion value between gas columns is over the predetermined value

preparation \*\*\*\*\* -- the abnormality diagnostic equipment of the internal combustion engine characterized by things.

[Claim 2]

It has a dispersion amendment means between gas columns to amend dispersion in the operational status between said internal combustion engine's gas columns based on said dispersion value between gas columns,

Said incorrect diagnostic prevention means is the abnormality diagnostic equipment of the internal combustion engine according to claim 1 characterized by performing prohibition of said abnormality diagnosis, or relaxation of an abnormality criterion when the dispersion amendment between gas columns by said dispersion amendment means between gas columns is not completed.

[Claim 3]

In the abnormality diagnostic equipment of the internal combustion engine having an abnormality diagnostic means to perform a predetermined abnormality diagnosis based on the output of the sensor which detects the information about the operational status of the internal combustion engine which has two or more gas columns,

A dispersion detection means between gas columns to calculate the dispersion value between gas columns showing dispersion in the operational status between said internal combustion engine's gas columns,

A dispersion amendment means between gas columns to amend dispersion in the operational status between said internal combustion engine's gas columns based on said dispersion value between gas columns,

An incorrect diagnostic prevention means to perform prohibition of the abnormality diagnosis by said abnormality diagnostic means, or relaxation of an abnormality criterion when the dispersion amendment between gas columns by said dispersion amendment means between gas columns is not completed

preparation \*\*\*\*\* -- the abnormality diagnostic equipment of the internal combustion engine characterized by things.

[Claim 4]

Said incorrect diagnostic prevention means is the abnormality diagnostic equipment of the internal combustion engine according to claim 2 or 3 with which after completion of the dispersion

amendment between gas columns by said dispersion amendment means between gas columns is characterized by continuing prohibition of said abnormality diagnosis, or relaxation of an abnormality criterion until a predetermined period passes.

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**DETAILED DESCRIPTION**

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**[Detailed Description of the Invention]**

[0001]

**[Field of the Invention]**

This invention relates to the abnormality diagnostic equipment of the internal combustion engine which performs a predetermined abnormality diagnosis based on the output of the sensor which detects the information about an internal combustion engine's operational status.

[0002]

**[Description of the Prior Art]**

While carrying the various sensors which detect various kinds of information (for example, an inhalation air content, the pressure-of-induction-pipe force, rotational speed, an air-fuel ratio, etc.) about operational status and controlling fuel oil consumption (air-fuel ratio), ignition timing, etc. by the internal combustion engine with which recent years were electronics-control-ized based on the output of these various sensors, it is made to perform various kinds of abnormality diagnoses using the output of these various sensors. For example, there are some which diagnosed the existence of the abnormalities of this air-fuel ratio sensor based on the output of the air-fuel ratio sensor which detects the air-fuel ratio of an internal combustion engine's exhaust gas as indicated by the patent reference 1 (JP,9-166569,A).

[0003]

**[Patent reference 1]**

JP,9-166569,A (the 2nd page etc.)

[0004]

**[Problem(s) to be Solved by the Invention]**

However, in the internal combustion engine which has two or more gas columns, dispersion may arise in the operational status of each gas column according to the individual difference (components tolerance, tolerance with a group, etc.) of each gas column, secular change, etc. For this reason, if dispersion in the operational status between gas columns is large when performing various kinds of abnormality diagnoses based on the output of the sensor which detects the information (for example, an inhalation air content, the pressure-of-induction-pipe force, rotational speed, an air-fuel ratio, etc.) about an internal combustion engine's operational status, in response to that effect, the fluctuation in a cycle of a sensor output becomes large, and although the object of an abnormality diagnosis is normal, it may incorrect-diagnose as abnormalities.

[0005]

This invention is made in consideration of such a situation, therefore it can prevent that the purpose incorrect-diagnoses turbulence of the sensor output produced by dispersion between gas columns as the abnormalities for an abnormality diagnosis, and is in offering the control unit of the internal combustion engine which can raise abnormality accuracy.

[0006]

**[Means for Solving the Problem]**

In order to attain the above-mentioned purpose, the abnormality diagnostic equipment of the internal combustion engine of claim 1 of this invention is made to perform prohibition of the abnormality diagnosis by the abnormality diagnostic means, or relaxation of an abnormality criterion with an incorrect diagnostic prevention means, when the dispersion detection means between gas columns

detects the dispersion value between gas columns showing dispersion in the operational status between an internal combustion engine's gas columns and the dispersion value between gas columns is over the predetermined value. If it will be in the condition that turbulence of a sensor output exceeds abnormality judging level by dispersion between gas columns, since forbid an abnormality diagnosis or the dispersion value between gas columns which detected with the dispersion detection means between gas columns will ease an abnormality criterion exceeding a predetermined value, it can prevent incorrect-diagnosing turbulence of the sensor output which produces by dispersion between gas columns as the abnormalities for an abnormality diagnosis, and abnormality accuracy can raise with this configuration.

[0007]

Moreover, since dispersion between gas columns is still large, turbulence of a sensor output may exceed the usual abnormality judging level, until the dispersion amendment between gas columns is completed in the case of the system equipped with a dispersion amendment means between gas columns to amend dispersion in the operational status between an internal combustion engine's gas columns based on the dispersion value between gas columns.

[0008]

Then, like claims 2 and 3, when the dispersion amendment between gas columns is not completed, it may be made to perform prohibition of an abnormality diagnosis, or relaxation of an abnormality criterion. If it does in this way, it can prevent incorrect-diagnosing turbulence of the sensor output which is before completion of the dispersion amendment between gas columns, and is produced when dispersion between gas columns is still large as the abnormalities for an abnormality diagnosis, and abnormality accuracy can be raised.

[0009]

Moreover, you may make it after completion of the dispersion amendment between gas columns continue prohibition of an abnormality diagnosis, or relaxation of an abnormality criterion like claim 4, since time amount may be taken for a while by the time dispersion between gas columns actually becomes small enough, after performing dispersion amendment between gas columns until a predetermined period passes. If it does in this way, prohibition or an abnormality criterion can be eased for an abnormality diagnosis also at the period when it is immediately after completion of the dispersion amendment between gas columns at, and dispersion between gas columns may not be small enough, and an incorrect diagnosis can be prevented more certainly.

[0010]

[Embodiment of the Invention]

<<operation gestalt (1) >>

Hereafter, the operation gestalt (1) of this invention is explained based on drawing 1 thru/or drawing 7. First, based on drawing 1, the outline configuration of the whole engine control system is explained. the engine 11 of a 4-cylinder which is an internal combustion engine -- the 1cylinder#1-the 4th -- it has four gas columns of cylinder #4, and an air cleaner 13 is formed in the maximum upstream section of the inlet pipe 12 of this engine 11, and the air flow meter 14 which detects an inhalation air content to the downstream of this air cleaner 13 is formed in it. The throttle valve 15 by which opening accommodation is carried out with a DC motor etc., and the throttle opening sensor 16 which detects throttle opening are formed in the downstream of this air flow meter 14.

[0011]

Moreover, a surge tank 17 is formed in the downstream of a throttle valve 15, and the pressure-of-induction-pipe force sensor 18 which detects the pressure-of-induction-pipe force to this surge tank 17 is formed in it. Moreover, the inlet manifold 19 which introduces air into each gas column of an engine 11 is formed in a surge tank 17, and the fuel injection valve 20 which injects a fuel, respectively is attached in it near the suction port of the inlet manifold 19 of each gas column.

Moreover, an ignition plug 21 is attached in the cylinder head of an engine 11 for every gas column, and it is lit by the spark discharge of each point fire plug 21 by the gaseous mixture in a cylinder.

[0012]

On the other hand, the catalysts 23, such as a three way component catalyst which purifies CO, HC, NOx, etc. in an exhaust gas, are formed in the exhaust pipe 22 of an engine 11, and the discharge gas sensors 24 (an air-fuel ratio sensor, oxygen sensor, etc.) which detect the air-fuel ratio of an exhaust

gas, or Lean/Rich to the upstream of this catalyst 23 are formed in it. Moreover, whenever the coolant temperature sensor 25 which detects cooling water temperature, and the crankshaft of an engine 11 carry out fixed crank angle (for example, 30degree-CA) rotation, the crank angle sensor 26 which outputs a pulse signal is attached in the cylinder block of an engine 11. A crank angle and an engine speed are detected based on the output signal of this crank angle sensor 26.

[0013]

The output of the various sensors mentioned above is inputted into the engine control circuit (it is written as "ECU" below) 27. This ECU27 is performing various kinds of engine control programs which were constituted as a subject and memorized by built-in ROM (storage) in the microcomputer, and controls the fuel oil consumption of a fuel injection valve 20, and the ignition timing of an ignition plug 21 according to an engine operation condition.

[0014]

ECU27 is air-fuel ratio lambdas of the exhaust gas detected with the discharge gas sensor 24 by performing the air-fuel ratio feedback control program which is not illustrated in that case. The air-fuel ratio correction factor FAF is computed so that it may be made in agreement with target air-fuel ratio lambdatg, and fuel oil consumption is computed using this air-fuel ratio correction factor FAF.

[0015]

Furthermore, ECU27 is performing the abnormality diagnostic program in a discharge gas sensor shown in drawing 2 mentioned later, and when target air-fuel ratio lambdatg changes, the existence of the abnormalities (failure, degradation, etc.) of the discharge gas sensor 24 is diagnosed by whether the ratio (delta FAF/deltalambdatg) of the variation deltalambdatg of target air-fuel ratio lambdatg and variation deltaFAF of the air-fuel ratio correction factor FAF is in the predetermined range (KCGL-KCGH).

[0016]

However, if dispersion in the operational status between gas columns is large, there is a possibility that the fluctuation in a cycle of discharge gas sensor 24 output may become large in response to the effect, and an abnormality diagnostic parameter (for example, delta FAF/deltalambdatg) may exceed an abnormality decision value (for example, the lower limit KCGL or upper limit (KCGH) of the predetermined range), and although the discharge gas sensor 24 is normal, it may incorrect-diagnose as those with abnormalities.

[0017]

Then, ECU27 is performing the dispersion detection program between gas columns shown in drawing 3 and drawing 4 which are mentioned later, is performing the dispersion amendment program between gas columns which computes the dispersion value DEV between gas columns showing dispersion in the operational status between the gas columns of an engine 11, and shows it to drawing 6 mentioned later, and amends dispersion in the operational status between the gas columns of an engine 11 based on the dispersion value DEV between gas columns.

[0018]

And it prevents incorrect-diagnosing turbulence of the output of the discharge gas sensor 24 which forbids an abnormality diagnosis of the discharge gas sensor 24, and is produced by dispersion between gas columns by performing the incorrect diagnostic prevention program shown in drawing 7 mentioned later when the dispersion value DEV between gas columns has crossed the predetermined range, or when the dispersion amendment between gas columns is not completed as the abnormalities of the discharge gas sensor 24. Hereafter, the contents of processing of each program which ECU27 performs are explained.

[0019]

[Abnormality diagnostic program in a discharge gas sensor]

The abnormality diagnostic program in a discharge gas sensor shown in drawing 2 is performed for every fuel-injection timing, and plays a role of an abnormality diagnostic means as used in the field of a claim. If this program is started -- target air-fuel ratio lambdatg (i-1) of the current target air-fuel ratio lambdatg and last time in step 101 first It judges whether the absolute value of a difference is beyond the predetermined decision value Klambdatg. It is  $|\lambda_{tg} - \lambda_{tg(i-1)}|$ . If it is  $< K_{lambdatg}$ , it will judge that target air-fuel ratio lambdatg is not changing, will progress to step 105, and will judge whether it is set to "1" as which the target air-fuel ratio change flag X means that

target air-fuel ratio lambdatg ends [ change detection ]. This program is ended without performing subsequent processings, if the target air-fuel ratio change flag X is not set to "1."  
[0020]

then, |lambda tg-lambda tg (i-1) the step 103 when set to |>=Klambdatg, after judging that target air-fuel ratio lambdatg changed, progressing to step 102 and setting the target air-fuel ratio change flag X to "1" -- progressing -- target air-fuel ratio lambdatg 1 time before current target air-fuel ratio lambdatg (i-1) The variation deltalambdatg of target air-fuel ratio lambdatg is computed by subtracting.

Deltalambdatg=lambda tg-lambda tg (i-1)

[0021]

Then, it progresses to step 104, the air-fuel ratio correction factor FAF at that time is memorized in the memory (not shown) of ECU27 as an air-fuel ratio correction factor FAFBF before changing, and this program is ended.

[0022]

and -- if it is judged with "No" at step 101, it progresses to step 105 and the target air-fuel ratio change flag X is set to "1" after change of target air-fuel ratio lambdatg, whenever this program is started -- step 106 -- progressing -- current target air-fuel ratio lambdatg and target air-fuel ratio lambdatg of 1 time ago (i-1) A difference is added to deltalambdatg till then and the storage value of deltalambdatg is updated.

Deltalambdatg=deltalambdatg+ {lambda tg-lambda tg (i-1) }

[0023]

then, the step 107 -- progressing -- the current air-fuel ratio correction factor FAF and air-fuel ratio correction factor FAF (i-1) of 1 time ago It judges whether the absolute value of a difference turned into below the predetermined value KFAF. And |FAF-FAF (i-1) When set to |<=KFAF (i.e., when completed as a predetermined value by the air-fuel ratio correction factor FAF), variation deltaFAF of the air-fuel ratio correction factor FAF is computed by progressing to step 108 and subtracting the air-fuel ratio correction factor FAFBF before change memorized at said step 104 from the current air-fuel ratio correction factor FAF.

deltaFAF=FAF-FAFBF

[0024]

Then, after progressing to step 109 and resetting the target air-fuel ratio change flag X to "0", it progresses to step 110 and judges whether the ratio of the absolute value of deltaFAF and the absolute value of deltalambdatg is predetermined within the limits  
(KCGL<=|deltaFAF|/|deltalambdatg|<=KCGH) (for example, KCGL=0.9, KCGH=1.1).

[0025]

Consequently, when judged with the ratio of the absolute value of deltaFAF and the absolute value of deltalambdatg being predetermined within the limits, it progresses to step 111, it judges with having no abnormalities of the discharge gas sensor 24 (normal), and this program is ended.

[0026]

On the other hand, when judged with the ratio of the absolute value of deltaFAF and the absolute value of deltalambdatg having separated from the predetermined range Progress to step 112 and it judges to be the abnormalities of the discharge gas sensor 24 (failure, degradation, etc.). While turning on the warning lamp (not shown) formed in the instrument panel of a driver's seat, or carrying out an alarm display to the alarm display section (not shown) and warning an operator The abnormality information (abnormality code) is memorized to the backup RAM of ECU27 (not shown), and this program is ended.

[0027]

[The dispersion detection program between gas columns]

The dispersion detection program between gas columns shown in drawing 3 and drawing 4 is performed a predetermined period after ON of an ignition switch (not shown), and plays a role of a dispersion detection means between gas columns as used in the field of a claim.

[0028]

Here, as shown in drawing 5, the wave of the pressure-of-induction-pipe force detected by the pressure-of-induction-pipe force sensor 18 turns into a pulsating wave reflecting the operational

status (an inhalation air content, a combustion condition, air-fuel ratio, etc.) of each gas column. Therefore, if the characteristic value of the minimal value of the pressure-of-induction-pipe force detected by the pressure-of-induction-pipe force sensor 18 for every crank angle range in which the effect of each gas column appears, the maximal value, the average, amplitude value, area, locus length, etc. is computed, since the characteristic value reflecting the operational status of each gas column of a pulsating wave is computable, if this characteristic value is used, the dispersion value between gas columns reflecting dispersion in the operational status of each gas column is computable.

[0029]

in addition, the 1- later mentioned in this program as shown in drawing 5 (a) in order to compute the dispersion value between gas columns using the minimal value of the pressure-of-induction-pipe force -- the 4th crank angle range -- respectively -- the 1- it is set up so that the field where the pressure-of-induction-pipe force serves as the minimal value under the effect of the 4th cylinder may be included.

[0030]

a \*\*\*\*\* [ that the execution condition of the dispersion detection between gas columns will be first satisfied at step 201 if this program is started ] -- a steady state (it is not a transient) \*\*\*\*\* -- etc. -- it judges. This program is ended without performing subsequent processings, if judged with the execution condition of the dispersion detection between gas columns being abortive.

[0031]

It judges whether the crank angle which progressed to step 202 and was detected at the above-mentioned step 201 on the other hand based on the output signal of the crank angle sensor 26 when judged with the execution condition of the dispersion detection between gas columns being satisfied is in the 1st crank angle range (the 1cylinder# crank angle range including the field where the pressure-of-induction-pipe force serves as the minimal value under the effect of 1). consequently, the minimal value PMmin of the pressure-of-induction-pipe [ progress to step 203 and ] force of crank angle within the limits of \*\* a 1st if judged with it being crank angle within the limits of \*\* a 1st the 1st -- the pressure-of-induction-pipe force minimal value PMmin of cylinder #1 (#1) \*\*\*\*\* -- it computes.

[0032]

On the other hand, when judged with a crank angle not being crank angle within the limits of \*\* a 1st at the above-mentioned step 202, it progresses to step 204 and judges whether a crank angle is in the 2nd crank angle range (the 2cylinder# crank angle range including the field where the pressure-of-induction-pipe force serves as the minimal value under the effect of 2). consequently, the minimal value PMmin of the pressure-of-induction-pipe [ progress to step 205 and ] force of crank angle within the limits of \*\* a 2nd if judged with it being crank angle within the limits of \*\* a 2nd the 2nd -- the pressure-of-induction-pipe force minimal value PMmin of cylinder #2 (#2) \*\*\*\*\* -- it computes.

[0033]

Moreover, when judged with a crank angle not being crank angle within the limits of \*\* a 2nd at the above-mentioned step 204, it progresses to step 206 and judges whether a crank angle is in the 3rd crank angle range (the 3cylinder# crank angle range including the field where the pressure-of-induction-pipe force serves as the minimal value under the effect of 3). consequently, the minimal value PMmin of the pressure-of-induction-pipe [ progress to step 207 and ] force of crank angle within the limits of \*\* a 3rd if judged with it being crank angle within the limits of \*\* a 3rd the 3rd - - the pressure-of-induction-pipe force minimal value PMmin of cylinder #3 (#3) \*\*\*\*\* -- it computes.

[0034]

moreover, when judged with a crank angle not being crank angle within the limits of \*\* a 3rd at the above-mentioned step 206 It is judged that a crank angle is in the 4th crank angle range (the 4cylinder# crank angle range including the field where the pressure-of-induction-pipe force serves as the minimal value under the effect of 4). the minimal value PMmin of the pressure-of-induction-pipe [ progress to step 208 and ] force of crank angle within the limits of \*\* a 4th the 4th -- the pressure-of-induction-pipe force minimal value PMmin of cylinder #4 (#4) \*\*\*\*\* -- it computes.

[0035]

then, the step 209 of drawing 4 -- progressing -- the pressure-of-induction-pipe force minimal value PMmin of all gas columns (#1) - PMmin (#4) The average AVEPMmin It computes.  
 $AVEPMmin = \{PMmin(\#1) + \dots + PMmin(\#4)\} / 4$

[0036]

Then, it progresses to step 210 and is the pressure-of-induction-pipe force minimal value PMmin of each gas column (#i). Average AVEPMmin It uses and the dispersion value DEV (#i) between gas columns of each gas column is computed by the degree type. Here, it is #i=#1-#4.  
 $DEV(\#i) = PMmin(\#i) - AVEPMmin$

[0037]

Then, it progresses to step 211 and judges whether the dispersion value DEV (#i) between gas columns of each gas column is predetermined within the limits ( $K1 \leq DEV(\#i) \leq K2$ ), respectively. Consequently, when judged with having separated from the predetermined range from at least one of all the dispersion values  $DEV(\#1) - DEV(\#4)$  between gas columns, it progresses to step 212, it sets to "1" which means that dispersion between gas columns is large in the dispersion flag XDEV between gas columns, and this program is ended.

[0038]

On the other hand, when judged with all the dispersion values  $DEV(\#1) - DEV(\#4)$  between gas columns being predetermined within the limits, it progresses to step 213, it resets to "0" which means that dispersion between gas columns is small in the dispersion flag XDEV between gas columns, and this program is ended.

[0039]

[The dispersion amendment program between gas columns]

The dispersion amendment program between gas columns shown in drawing 6 is performed a predetermined period after ON of an ignition switch, and plays a role of a dispersion amendment means between gas columns as used in the field of a claim. First, if this program is started, after reading the dispersion value DEV (#i) between gas columns of each gas column, it will progress to step 302 and the fuel-injection-duration correction factor FTAU of each gas column (#i) will be computed by the degree type at step 301, using the dispersion value DEV (#i) between gas columns of each gas column.

$FTAU(\#i) = DEV(\#i) + 1$

[0040]

Then, it progresses to step 303, the multiplication of the fuel-injection-duration correction factor FTAU of each gas column (#i) is carried out to the average fuel injection duration TAU of all the gas columns before amendment, and the last fuel injection duration TAU (#i) of each gas column is found.

$TAU(\#i) = TAU \times FTAU(\#i)$

By the above processing, air-fuel ratio dispersion between gas columns is made small by amending the fuel oil consumption of each gas column according to the dispersion value DEV (#i) between gas columns of each gas column.

[0041]

[Incorrect diagnostic prevention program]

The incorrect diagnostic prevention program shown in drawing 7 is performed a predetermined period after ON of an ignition switch, and plays a role of an incorrect diagnostic prevention means as used in the field of a claim. When this program is started, at step 401 first \*\*1 It judges whether it is that dispersion between gas columns is small (dispersion flag XDEV between gas columns = 0). Moreover, \*\*2 After the dispersion amendment between gas columns is completed, it judges whether predetermined periods (predetermined time, predetermined crank angle, etc.) passed.

[0042]

Consequently, when judged with dispersion between gas columns being large (dispersion flag XDEV between gas columns = 1), or when it is judged with it being before the predetermined period has passed since the completion of the dispersion amendment between gas columns By dispersion between gas columns, the output of the discharge gas sensor 24 is confused, and it judges that an abnormality diagnostic parameter (for example, delta FAF/deltalambdatg) may separate from a

normal range (KCGL-KCGH), and progresses to step 402, and an abnormality diagnosis of the discharge gas sensor 24 is forbidden. It prevents that this incorrect-diagnoses turbulence of the output of the discharge gas sensor 24 produced by dispersion between gas columns as the abnormalities of the discharge gas sensor 24.

[0043]

On the other hand, at the above-mentioned step 401, when judged with dispersion between gas columns being small, or when [ after the dispersion amendment between gas columns is completed ] it is judged with the predetermined period having passed, it progresses to step 403 and an abnormality diagnosis of the discharge gas sensor 24 is permitted.

[0044]

With this operation gestalt (1) explained above, since the abnormality diagnosis of the discharge gas sensor 24 was forbidden when dispersion between gas columns was large, it can prevent incorrect-diagnosing turbulence of the output of the discharge gas sensor 24 produced by dispersion between gas columns as the abnormalities of the discharge gas sensor 24, and the abnormality accuracy of the discharge gas sensor 24 can be raised.

[0045]

Moreover, until a predetermined period passes in consideration of taking time amount for a while by the time dispersion between gas columns actually becomes small enough with this operation gestalt (1), after performing dispersion amendment between gas columns also even in after completion of the dispersion amendment between gas columns Since prohibition of an abnormality diagnosis of the discharge gas sensor 24 was continued, an abnormality diagnosis can also be forbidden to the period when it is immediately after completion of the dispersion amendment between gas columns at, and dispersion between gas columns may not be small enough, and an incorrect diagnosis can be prevented more certainly at it.

[0046]

However, when it is not necessarily necessary to continue prohibition of an abnormality diagnosis until a predetermined period passes since the completion of the dispersion amendment between gas columns, and dispersion between gas columns becomes small promptly by dispersion amendment between gas columns, you may make it permit an abnormality diagnosis of the discharge gas sensor 24 immediately immediately after the completion of the dispersion amendment between gas columns.

[0047]

<<operation gestalt (2) >>

Next, the operation gestalt (2) of this invention is explained using drawing 8 thru/or drawing 10. Although the dispersion value between gas columns was computed with said operation gestalt (1) using the minimal value of the pressure-of-induction-pipe force, he is trying to compute the dispersion value between gas columns with this operation gestalt (2) using the maximal value of the pressure-of-induction-pipe force by performing the dispersion detection program between gas columns shown in drawing 8 and drawing 9 which are mentioned later.

[0048]

Moreover, although the abnormality diagnosis of the discharge gas sensor 24 was forbidden with said operation gestalt (1) for incorrect diagnostic prevention, he is trying to ease the abnormality criterion of the discharge gas sensor 24 with this operation gestalt (2) for incorrect diagnostic prevention by performing the incorrect diagnostic prevention program shown in drawing 10 mentioned later.

[0049]

[The dispersion detection program between gas columns]

the 1- later mentioned in the dispersion detection program between gas columns shown in drawing 8 and drawing 9 as shown in drawing 5 (b) in order to compute the dispersion value between gas columns using the maximal value of the pressure-of-induction-pipe force -- the 4th crank angle range -- respectively -- the 1- it is set up so that the field where the pressure-of-induction-pipe force serves as the maximal value under the effect of the 4th cylinder may be included.

[0050]

When judged with the execution condition of the dispersion detection between gas columns being

satisfied at step 501 in this program, A crank angle at the time in the 1st crank angle range (the 1cylinder# crank angle range including the field where the pressure-of-induction-pipe force serves as the maximal value under the effect of 1) this -- the maximal value PMmax of the pressure-of-induction-pipe force of crank angle within the limits of \*\* a 1st the 1st -- the pressure-of-induction-pipe force maximal value PMmax of cylinder #1 (#1) \*\*\*\*\* -- it computes (steps 502 and 503).  
[0051]

on the other hand -- a crank angle -- the time in the 2nd crank angle range (the 2cylinder# crank angle range including the field where the pressure-of-induction-pipe force serves as the maximal value under the effect of 2) -- this -- the maximal value PMmax of the pressure-of-induction-pipe force of crank angle within the limits of \*\* a 2nd the 2nd -- the pressure-of-induction-pipe force maximal value PMmax of cylinder #2 (#2) \*\*\*\*\* -- it computes (steps 504 and 505).

[0052]

moreover, a crank angle -- the time in the 3rd crank angle range (the 3cylinder# crank angle range including the field where the pressure-of-induction-pipe force serves as the maximal value under the effect of 3) -- this -- the maximal value PMmax of the pressure-of-induction-pipe force of crank angle within the limits of \*\* a 3rd the 3rd -- the pressure-of-induction-pipe force maximal value PMmax of cylinder #3 (#3) \*\*\*\*\* -- it computes (steps 506 and 507).

[0053]

moreover, a crank angle -- the time in the 4th crank angle range (the 4cylinder# crank angle range including the field where the pressure-of-induction-pipe force serves as the maximal value under the effect of 4) -- this -- the maximal value PMmax of the pressure-of-induction-pipe force of crank angle within the limits of \*\* a 4th the 4th -- the pressure-of-induction-pipe force maximal value PMmax of cylinder #4 (#4) \*\*\*\*\* -- it computes (step 508).

[0054]

then, the step 509 of drawing 9 -- progressing -- the pressure-of-induction-pipe force maximal value PMmax of all gas columns (#1) - PMmax (#4) The average AVEPMmax It computes.

$$\text{AVEPMmax} = \{\text{PMmax}(\#1) + \dots + \text{PMmax}(\#4)\} / 4$$

[0055]

Then, it progresses to step 510 and is the pressure-of-induction-pipe force maximal value PMmax of each gas column (#i). Average AVEPMmax It uses and the dispersion value DEV (#i) between gas columns of each gas column is computed by the degree type.

$$\text{DEV}(\#i) = \text{PMmax}(\#i) - \text{AVEPMmax}$$

[0056]

It progresses to step 511. Then, the dispersion value DEV (#i) between gas columns of each gas column When it judges whether it is in the predetermined range (K1-K2), respectively and is judged with having crossed at least one predetermined range among all the dispersion values DEV (#1)-DEV (#4) between gas columns It progresses to step 512 and the dispersion flag XDEV between gas columns is set to "1", when judged with all the dispersion values DEV (#1)-DEV (#4) between gas columns being predetermined within the limits, it progresses to step 513 and the dispersion flag XDEV between gas columns is reset to "0."

[0057]

[Incorrect diagnostic prevention program]

In the incorrect diagnostic prevention program shown in drawing 10, at step 601, first \*\*1 It judges whether it is that dispersion between gas columns is small (dispersion flag XDEVbetween gas columns = 0). Moreover, \*\*2 It judges whether the dispersion amendment between gas columns was completed.

[0058]

Consequently, when judged with dispersion between gas columns being large (dispersion flag XDEVbetween gas columns = 1), or when judged [ having not completed the dispersion amendment between gas columns, and ] The output of the discharge gas sensor 24 is confused by dispersion between gas columns, and it is judged that an abnormality diagnostic parameter (for example, delta FAF/deltalambdatg) may separate from a normal range (a lower limit KCGL - a upper limit KCGH). It progresses to step 602, the lower limit KCGL of a normal range (abnormality decision value) is changed into the lower limit for incorrect diagnostic prevention (KCGL-alpha), a upper limit KCGH

(abnormality decision value) is changed into the upper limit for incorrect diagnostic prevention (KCGH+beta), the width of face of a normal range is expanded, and an abnormality criterion is eased. It prevents that this incorrect-diagnoses turbulence of the output of the discharge gas sensor 24 produced by dispersion between gas columns as the abnormalities of the discharge gas sensor 24. [0059]

On the other hand, at the above-mentioned step 601, when judged with dispersion between gas columns being small, or when it is judged with the dispersion amendment between gas columns having been completed, it progresses to step 603 and the lower limit (abnormality decision value) and upper limit (abnormality decision value) of a normal range are returned to the usual values KCGL and KCGH.

[0060]

With this operation gestalt (2) explained above, since the width of face of a normal range is expanded and the abnormality criterion was eased when having completed neither the time when dispersion between gas columns is large, nor the dispersion amendment between gas columns, it can prevent incorrect-diagnosing turbulence of the output of the discharge gas sensor 24 produced by dispersion between gas columns as the abnormalities of the discharge gas sensor 24, and the abnormality accuracy of the discharge gas sensor 24 can be raised.

[0061]

In addition, although the abnormality decision value (the lower limit and upper limit of a normal range) was changed with this operation gestalt (2) in order to ease an abnormality criterion, you may make it change other abnormality criteria, such as amending an abnormality diagnostic parameter (for example, delta FAF/deltalambdatg), or amending the output of the discharge gas sensor 24.

[0062]

Moreover, you may make it after the completion of the dispersion amendment between gas columns as well as said operation gestalt (1) continue relaxation of an abnormality criterion also in this operation gestalt (2) until a predetermined period passes.

[0063]

Moreover, although this invention was applied to the abnormality diagnosis of the discharge gas sensor 24 in each above-mentioned operation gestalt (1) and (2) The catalyst de-activation diagnosis this invention is not limited to this, for example, using the output of the discharge gas sensor 24, An abnormality diagnosis of the air flow meter 14 using the output of an air flow meter 14, An abnormality diagnosis of the pressure-of-induction-pipe force sensor 18 using the output of the pressure-of-induction-pipe force sensor 18, This invention is applicable to the various abnormality diagnoses influenced of dispersion between gas columns, such as an abnormality diagnosis of the catalyst early warming-up system using at least one output in an air flow meter 14, the pressure-of-induction-pipe force sensor 18, and the discharge gas sensor 24, and an abnormality diagnosis of the Air Fuel Ratio Control system.

[0064]

Moreover, although the dispersion value between gas columns was computed based on the maximal value or the minimal value for every predetermined period of the pressure-of-induction-pipe force, the calculation approach of the dispersion value between gas columns may be changed suitably, for example, you may make it compute the dispersion value between gas columns in each above-mentioned operation gestalt (1) and (2) based on the average for every predetermined period of the pressure-of-induction-pipe force, amplitude value, area, locus length, etc. Moreover, it replaces with the pressure-of-induction-pipe force, and you may make it compute the dispersion value between gas columns based on an inhalation air content, cylinder internal pressure, rotational speed, the ion current, an air-fuel ratio, etc.

[0065]

Moreover, although dispersion between gas columns was amended by amending fuel oil consumption for every gas column each above-mentioned operation gestalt (1) and (2), the amendment approach of dispersion between gas columns may be changed suitably, for example, it amends an inhalation air content for every gas column, and you may make it amend ignition timing for every gas column, or amend dispersion between gas columns.

[0066]

In addition, the applicability of this invention is not limited to the engine of a 4-cylinder, but may apply this invention to two or more cylinder engine below 5 cylinders or more or a 3 cylinder.

[Brief Description of the Drawings]

[Drawing 1] The outline block diagram of the whole engine control system in the operation gestalt (1) of this invention

[Drawing 2] The flow chart which shows the flow of processing of the abnormality diagnostic program in a discharge gas sensor of an operation gestalt (1)

[Drawing 3] The flow chart which shows the flow of processing of the dispersion detection program between gas columns of an operation gestalt (1) (the 1)

[Drawing 4] The flow chart which shows the flow of processing of the dispersion detection program between gas columns of an operation gestalt (1) (the 2)

[Drawing 5] The timing diagram which shows the behavior of the pressure-of-induction-pipe force

[Drawing 6] The flow chart which shows the flow of processing of the dispersion amendment program between gas columns of an operation gestalt (1)

[Drawing 7] The flow chart which shows the flow of processing of the incorrect diagnostic prevention program of an operation gestalt (1)

[Drawing 8] The flow chart which shows the flow of processing of the dispersion detection program between gas columns of an operation gestalt (2) (the 1)

[Drawing 9] The flow chart which shows the flow of processing of the dispersion detection program between gas columns of an operation gestalt (2) (the 2)

[Drawing 10] The flow chart which shows the flow of processing of the incorrect diagnostic prevention program of an operation gestalt (2)

[Description of Notations]

11 [ -- A throttle valve, 18 / -- A pressure-of-induction-pipe force sensor, 20 / -- A fuel injection valve, 21 / -- An ignition plug, 22 / -- An exhaust pipe, 24 / -- A discharge gas sensor, 26 / -- A crank angle sensor, 27 / -- ECU (an abnormality diagnostic means, the dispersion detection means between gas columns the dispersion amendment means between gas columns incorrect diagnostic prevention means). ] -- An engine (internal combustion engine), 12 -- An inlet pipe, 14 -- An air flow meter, 15

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[Translation done.]

**\* NOTICES \***

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2. \*\*\*\* shows the word which can not be translated.
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**DESCRIPTION OF DRAWINGS**

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**[Brief Description of the Drawings]**

[Drawing 1] The outline block diagram of the whole engine control system in the operation gestalt (1) of this invention

[Drawing 2] The flow chart which shows the flow of processing of the abnormality diagnostic program in a discharge gas sensor of an operation gestalt (1)

[Drawing 3] The flow chart which shows the flow of processing of the dispersion detection program between gas columns of an operation gestalt (1) (the 1)

[Drawing 4] The flow chart which shows the flow of processing of the dispersion detection program between gas columns of an operation gestalt (1) (the 2)

[Drawing 5] The timing diagram which shows the behavior of the pressure-of-induction-pipe force

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[Drawing 9] The flow chart which shows the flow of processing of the dispersion detection program between gas columns of an operation gestalt (2) (the 2)

[Drawing 10] The flow chart which shows the flow of processing of the incorrect diagnostic prevention program of an operation gestalt (2)

**[Description of Notations]**

11 [ -- A throttle valve, 18 / -- A pressure-of-induction-pipe force sensor, 20 / -- A fuel injection valve, 21 / -- An ignition plug, 22 / -- An exhaust pipe, 24 / -- A discharge gas sensor, 26 / -- A crank angle sensor, 27 / -- ECU ] -- An engine (internal combustion engine), 12 -- An inlet pipe, 14 -- An air flow meter, 15

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[Translation done.]

**\* NOTICES \***

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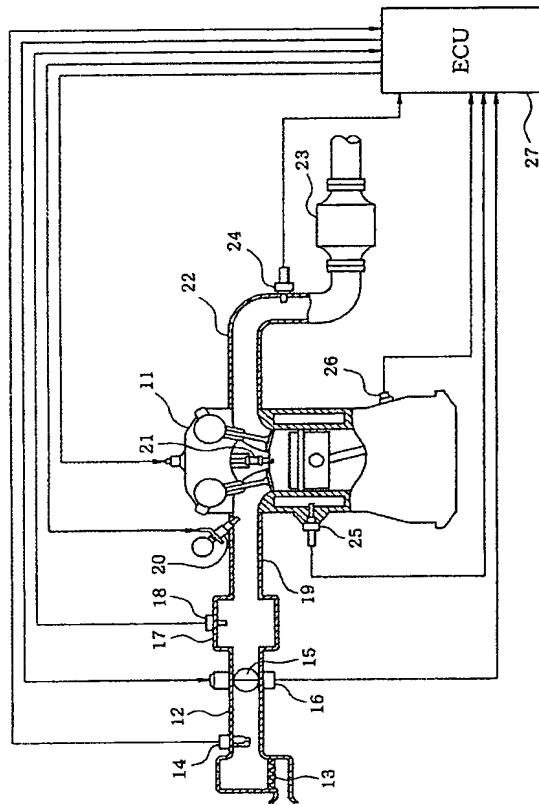
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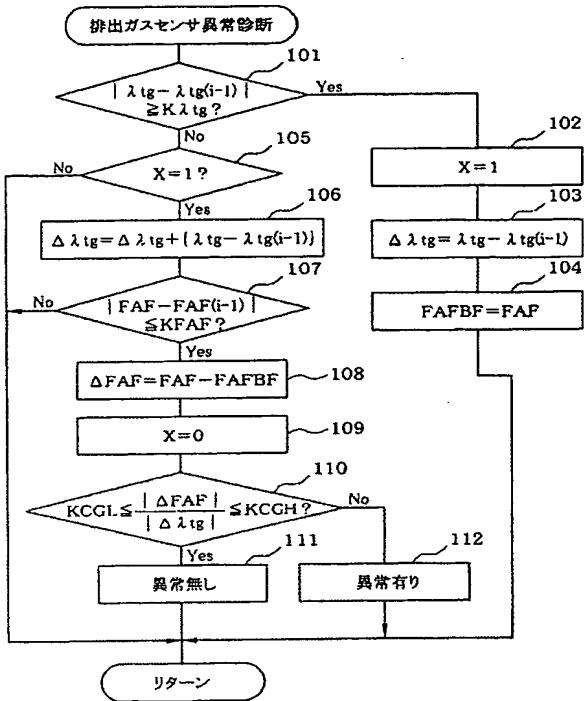
**DRAWINGS**

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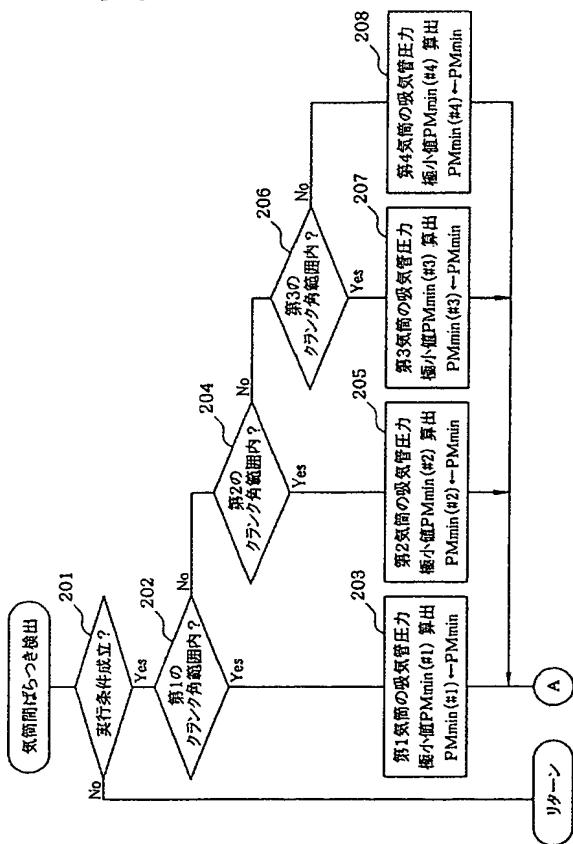
[Drawing 1]



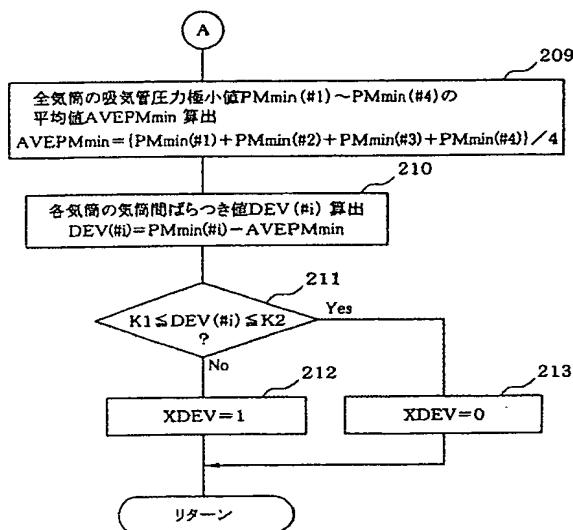
[Drawing 2]



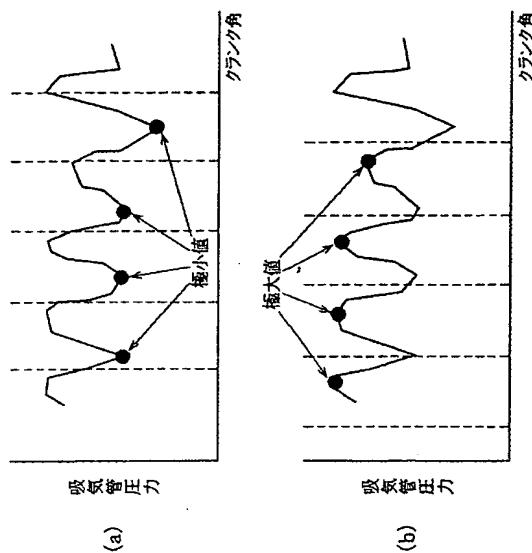
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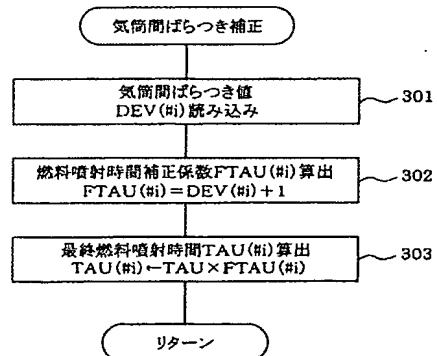
[Drawing 4]



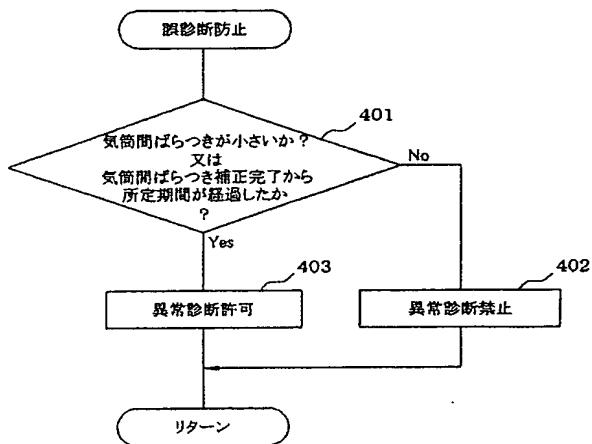
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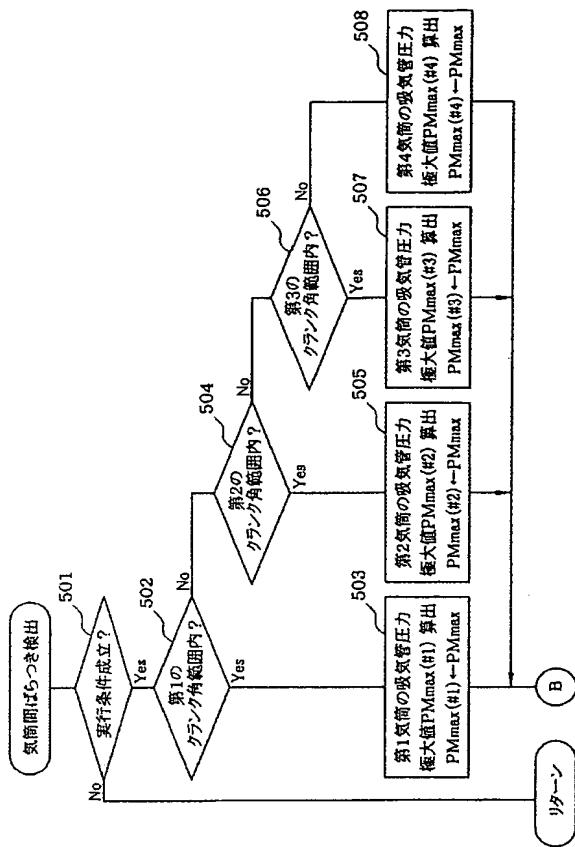
[Drawing 6]



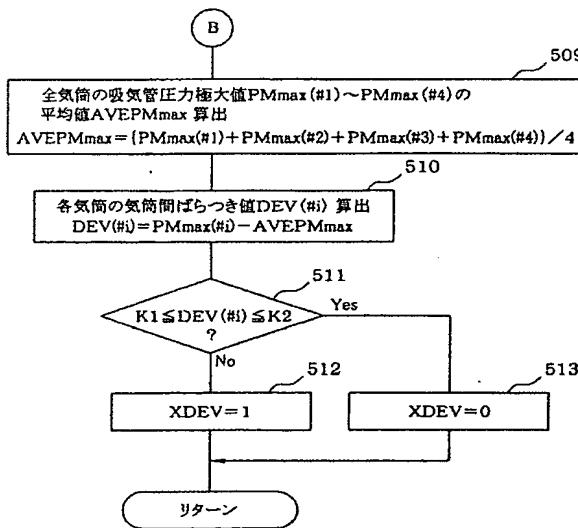
[Drawing 7]



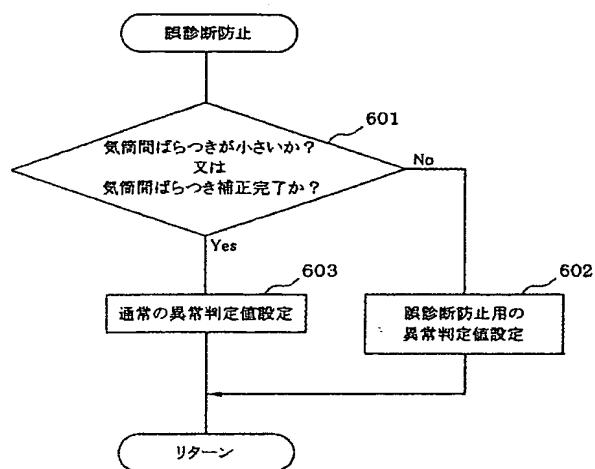
[Drawing 8]



[Drawing 9]



[Drawing 10]

[Translation done.]

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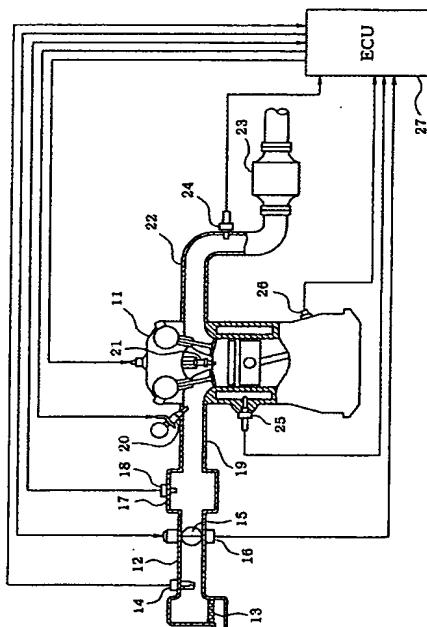
(54)【発明の名称】内燃機関の異常診断装置

## (57)【要約】

【課題】エンジンの気筒間ばらつきによって生じた排出ガスセンサの出力の乱れを排出ガスセンサの異常と誤診断することを防止できるようにする。

【解決手段】吸気管圧力センサ18で検出した吸気管圧力等の挙動に基づいて各気筒毎に気筒間ばらつき値を算出し、各気筒の気筒間ばらつき値に基づいて各気筒毎に燃料噴射量等を補正することで気筒間ばらつきを補正する。エンジン運転中に、気筒間ばらつき値が所定値を越えているとき、又は、気筒間ばらつき補正が完了するまでは、気筒間ばらつきによって生じた排出ガスセンサ24の出力の乱れが正常範囲を越えてしまう可能性があると判断して、排出ガスセンサ24の異常診断を禁止したり、或は、異常判定基準を緩和する。これにより、気筒間ばらつきによって生じた排出ガスセンサの出力の乱れを排出ガスセンサの異常と誤診断することを防止する。

【選択図】 図1



**【特許請求の範囲】****【請求項 1】**

複数の気筒を有する内燃機関の運転状態に関する情報を検出するセンサの出力に基づいて所定の異常診断を行う異常診断手段を備えた内燃機関の異常診断装置において、前記内燃機関の気筒間の運転状態のばらつきを表す気筒間ばらつき値を求める気筒間ばらつき検出手段と、

前記気筒間ばらつき値が所定値を越えているときに、前記異常診断手段による異常診断の禁止又は異常判定基準の緩和を実行する誤診断防止手段とを備えていることを特徴とする内燃機関の異常診断装置。

**【請求項 2】**

前記気筒間ばらつき値に基づいて前記内燃機関の気筒間の運転状態のばらつきを補正する気筒間ばらつき補正手段を備え、

前記誤診断防止手段は、前記気筒間ばらつき補正手段による気筒間ばらつき補正が完了していないときに、前記異常診断の禁止又は異常判定基準の緩和を実行することを特徴とする請求項 1 に記載の内燃機関の異常診断装置。

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**【請求項 3】**

複数の気筒を有する内燃機関の運転状態に関する情報を検出するセンサの出力に基づいて所定の異常診断を行う異常診断手段を備えた内燃機関の異常診断装置において、前記内燃機関の気筒間の運転状態のばらつきを表す気筒間ばらつき値を求める気筒間ばらつき検出手段と、

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前記気筒間ばらつき値に基づいて前記内燃機関の気筒間の運転状態のばらつきを補正する気筒間ばらつき補正手段と、

前記気筒間ばらつき補正手段による気筒間ばらつき補正が完了していないときに、前記異常診断手段による異常診断の禁止又は異常判定基準の緩和を実行する誤診断防止手段とを備えていることを特徴とする内燃機関の異常診断装置。

**【請求項 4】**

前記誤診断防止手段は、前記気筒間ばらつき補正手段による気筒間ばらつき補正の完了後も所定期間が経過するまで、前記異常診断の禁止又は異常判定基準の緩和を継続することを特徴とする請求項 2 又は 3 に記載の内燃機関の異常診断装置。

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**【発明の詳細な説明】****【0001】****【発明の属する技術分野】**

本発明は、内燃機関の運転状態に関する情報を検出するセンサの出力に基づいて所定の異常診断を行う内燃機関の異常診断装置に関するものである。

**【0002】****【従来の技術】**

近年の電子制御化された内燃機関では、運転状態に関する各種の情報（例えば吸入空気量、吸気管圧力、回転速度、空燃比等）を検出する各種センサを搭載し、これら各種センサの出力に基づいて燃料噴射量（空燃比）や点火時期等を制御すると共に、これら各種センサの出力をを利用して各種の異常診断を行うようにしている。例えば、特許文献 1（特開平 9-166569 号公報）に記載されているように、内燃機関の排出ガスの空燃比を検出する空燃比センサの出力に基づいて該空燃比センサの異常の有無を診断するようにしたものががある。

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**【0003】****【特許文献 1】**

特開平 9-166569 号公報（第 2 頁等）

**【0004】****【発明が解決しようとする課題】**

ところが、複数の気筒を有する内燃機関では、各気筒の個体差（部品公差、組付公差等）や経年変化等によって各気筒の運転状態にはらつきが生じることがある。このため、内燃

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機関の運転状態に関する情報（例えば吸入空気量、吸気管圧力、回転速度、空燃比等）を検出するセンサの出力に基づいて各種の異常診断を行う場合に、気筒間の運転状態のばらつきが大きいと、その影響を受けてセンサ出力のサイクル内変動が大きくなってしまい、異常診断の対象が正常であるにも拘らず異常と誤診断してしまう可能性がある。

### 【0005】

本発明はこのような事情を考慮してなされたものであり、従ってその目的は、気筒間ばらつきによって生じるセンサ出力の乱れを異常診断対象の異常と誤診断することを防止することができ、異常診断精度を向上させることができると内燃機関の制御装置を提供することにある。

### 【0006】

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#### 【課題を解決するための手段】

上記目的を達成するために、本発明の請求項1の内燃機関の異常診断装置は、内燃機関の気筒間の運転状態のばらつきを表す気筒間ばらつき値を気筒間ばらつき検出手段により検出し、気筒間ばらつき値が所定値を越えているときに、異常診断手段による異常診断の禁止又は異常判定基準の緩和を誤診断防止手段により実行するようにしたものである。この構成では、気筒間ばらつきによってセンサ出力の乱れが異常判定レベルを越えるような状態になれば、気筒間ばらつき検出手段により検出した気筒間ばらつき値が所定値を越えて異常診断を禁止したり又は異常判定基準を緩和するため、気筒間ばらつきによって生じるセンサ出力の乱れを異常診断対象の異常と誤診断することを防止することができ、異常診断精度を向上させることができる。

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### 【0007】

また、気筒間ばらつき値に基づいて内燃機関の気筒間の運転状態のばらつきを補正する気筒間ばらつき補正手段を備えたシステムの場合、気筒間ばらつき補正が完了するまでは、まだ気筒間ばらつきが大きいために、センサ出力の乱れが通常の異常判定レベルを越えてしまう可能性がある。

### 【0008】

そこで、請求項2、3のように、気筒間ばらつき補正が完了していないときに、異常診断の禁止又は異常判定基準の緩和を実行するようにしても良い。このようにすれば、気筒間ばらつき補正の完了前で、まだ気筒間ばらつきが大きいときに生じるセンサ出力の乱れを異常診断対象の異常と誤診断することを防止でき、異常診断精度を向上させることができる。

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### 【0009】

また、気筒間ばらつき補正を実行してから実際に気筒間ばらつきが十分に小さくなるまでには暫く時間が掛かることがあるため、請求項4のように、気筒間ばらつき補正の完了後も所定期間が経過するまで、異常診断の禁止又は異常判定基準の緩和を継続するようにしても良い。このようにすれば、気筒間ばらつき補正の完了直後で気筒間ばらつきが十分に小さくなっていない可能性がある期間にも異常診断を禁止又は異常判定基準を緩和して、より確実に誤診断を防止することができる。

### 【0010】

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#### 【発明の実施の形態】

##### 《実施形態(1)》

以下、本発明の実施形態(1)を図1乃至図7に基づいて説明する。まず、図1に基づいてエンジン制御システム全体の概略構成を説明する。内燃機関である例えば4気筒のエンジン11は、第1気筒#1～第4気筒#4の4つの気筒を有し、このエンジン11の吸気管12の最上流部には、エアクリーナ13が設けられ、このエアクリーナ13の下流側に、吸入空気量を検出するエアフローメータ14が設けられている。このエアフローメータ14の下流側には、DCモータ等によって開度調節されるスロットルバルブ15とスロットル開度を検出するスロットル開度センサ16とが設けられている。

### 【0011】

また、スロットルバルブ15の下流側には、サージタンク17が設けられ、このサージタ

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シク17に、吸気管圧力を検出する吸気管圧力センサ18が設けられている。また、サイジタンク17には、エンジン11の各気筒に空気を導入する吸気マニホールド19が設けられ、各気筒の吸気マニホールド19の吸気ポート近傍に、それぞれ燃料を噴射する燃料噴射弁20が取り付けられている。また、エンジン11のシリンダヘッドには、各気筒毎に点火プラグ21が取り付けられ、各点火プラグ21の火花放電によって筒内の混合気に着火される。

#### 【0012】

一方、エンジン11の排気管22には、排出ガス中のCO, HC, NO<sub>x</sub>等を浄化する三元触媒等の触媒23が設けられ、この触媒23の上流側に、排出ガスの空燃比又はリーン／リッチ等を検出する排出ガスセンサ24（空燃比センサ、酸素センサ等）が設けられている。また、エンジン11のシリンダブロックには、冷却水温を検出する水温センサ25や、エンジン11のクランク軸が一定クランク角（例えば30°C A）回転する毎にパルス信号を出力するクランク角センサ26が取り付けられている。このクランク角センサ26の出力信号に基づいてクランク角やエンジン回転速度が検出される。

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#### 【0013】

前述した各種センサの出力は、エンジン制御回路（以下「ECU」と表記する）27に入力される。このECU27は、マイクロコンピュータを主体として構成され、内蔵されたROM（記憶媒体）に記憶された各種のエンジン制御プログラムを実行することで、エンジン運転状態に応じて燃料噴射弁20の燃料噴射量や点火プラグ21の点火時期を制御する。

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#### 【0014】

その際、ECU27は、図示しない空燃比フィードバック制御プログラムを実行することで、排出ガスセンサ24で検出した排出ガスの空燃比 $\lambda_s$ を目標空燃比 $\lambda_{tg}$ に一致させるように空燃比補正係数F AFを算出し、この空燃比補正係数F AFを用いて燃料噴射量を算出する。

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#### 【0015】

更に、ECU27は、後述する図2に示す排出ガスセンサ異常診断プログラムを実行することで、目標空燃比 $\lambda_{tg}$ が変化したときに、目標空燃比 $\lambda_{tg}$ の変化量 $\Delta\lambda_{tg}$ と空燃比補正係数F AFの変化量 $\Delta F AF$ との比（ $\Delta F AF / \Delta\lambda_{tg}$ ）が所定範囲（K C G L～K C G H）内であるか否かによって排出ガスセンサ24の異常（故障、劣化等）の有無を診断する。

#### 【0016】

しかし、気筒間の運転状態のばらつきが大きいと、その影響を受けて排出ガスセンサ24出力のサイクル内変動が大きくなつて異常診断パラメータ（例えば $\Delta F AF / \Delta\lambda_{tg}$ ）が異常判定値（例えば所定範囲の下限値K C G L又は上限値K C G H）を越えてしまうおそれがあり、排出ガスセンサ24が正常であるにも拘らず異常有りと誤診断してしまう可能性がある。

#### 【0017】

そこで、ECU27は、後述する図3及び図4に示す気筒間ばらつき検出プログラムを実行することで、エンジン11の気筒間の運転状態のばらつきを表す気筒間ばらつき値D E Vを算出し、後述する図6に示す気筒間ばらつき補正プログラムを実行することで、気筒間ばらつき値D E Vに基づいてエンジン11の気筒間の運転状態のばらつきを補正する。

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#### 【0018】

そして、後述する図7に示す誤診断防止プログラムを実行することで、気筒間ばらつき値D E Vが所定範囲を越えているとき、又は、気筒間ばらつき補正が完了していないとき、排出ガスセンサ24の異常診断を禁止して、気筒間ばらつきによって生じる排出ガスセンサ24の出力の乱れを排出ガスセンサ24の異常と誤診断してしまうことを防止する。以下、ECU27が実行する各プログラムの処理内容を説明する。

#### 【0019】

[排出ガスセンサ異常診断プログラム]

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図2に示す排出ガスセンサ異常診断プログラムは、例えば、燃料噴射タイミング毎に実行され、特許請求の範囲でいう異常診断手段としての役割を果たす。本プログラムが起動されると、まず、ステップ101で、現在の目標空燃比 $\lambda_{tg}$ と前回の目標空燃比 $\lambda_{tg}(i-1)$ との差の絶対値が所定の判定値 $K\lambda_{tg}$ 以上であるか否かを判定する。もし、 $|\lambda_{tg} - \lambda_{tg}(i-1)| < K\lambda_{tg}$ であれば、目標空燃比 $\lambda_{tg}$ が変化していないと判断して、ステップ105に進み、目標空燃比変化フラグXが目標空燃比 $\lambda_{tg}$ の変化検出済みを意味する「1」にセットされているか否かを判定する。目標空燃比変化フラグXが「1」にセットされていなければ、以降の処理を行うことなく、本プログラムを終了する。

#### 【0020】

その後、 $|\lambda_{tg} - \lambda_{tg}(i-1)| \geq K\lambda_{tg}$ になった時点で、目標空燃比 $\lambda_{tg}$ が変化したと判断して、ステップ102に進み、目標空燃比変化フラグXを「1」にセットした後、ステップ103に進み、現在の目標空燃比 $\lambda_{tg}$ から1回前の目標空燃比 $\lambda_{tg}(i-1)$ を減算して、目標空燃比 $\lambda_{tg}$ の変化量 $\Delta\lambda_{tg}$ を算出する。

$$\Delta\lambda_{tg} = \lambda_{tg} - \lambda_{tg}(i-1)$$

#### 【0021】

この後、ステップ104に進み、そのときの空燃比補正係数FAFを変化前の空燃比補正係数FAFBFとしてECU27のメモリ(図示せず)に記憶して、本プログラムを終了する。

#### 【0022】

そして、目標空燃比 $\lambda_{tg}$ の変化後に、本プログラムが起動される毎に、ステップ101で「No」と判定されてステップ105に進み、目標空燃比変化フラグXが「1」にセットされていれば、ステップ106に進み、現在の目標空燃比 $\lambda_{tg}$ と1回前の目標空燃比 $\lambda_{tg}(i-1)$ との差をそれまでの $\Delta\lambda_{tg}$ に加算して、 $\Delta\lambda_{tg}$ の記憶値を更新する。

$$\Delta\lambda_{tg} = \Delta\lambda_{tg} + \{\lambda_{tg} - \lambda_{tg}(i-1)\}$$

#### 【0023】

この後、ステップ107に進み、現在の空燃比補正係数FAFと1回前の空燃比補正係数FAF(i-1)との差の絶対値が所定値KFAF以下になったか否かを判定する。そして、 $|FAF - FAF(i-1)| \leq KFAF$ となったとき、つまり、空燃比補正係数FAFが所定の値に収束したときに、ステップ108に進み、現在の空燃比補正係数FAFから前記ステップ104で記憶した変化前の空燃比補正係数FAFBFを減算して、空燃比補正係数FAFの変化量 $\Delta FAF$ を算出する。

$$\Delta FAF = FAF - FAFBF$$

#### 【0024】

この後、ステップ109に進み、目標空燃比変化フラグXを「0」にリセットした後、ステップ110に進み、 $\Delta FAF$ の絶対値と $\Delta\lambda_{tg}$ の絶対値との比が所定範囲内( $KCG_L \leq |\Delta FAF| / |\Delta\lambda_{tg}| \leq KCG_H$ )であるか否かを判定する(例えば $KCG_L = 0.9$ 、 $KCG_H = 1.1$ )。

#### 【0025】

その結果、 $\Delta FAF$ の絶対値と $\Delta\lambda_{tg}$ の絶対値との比が所定範囲内であると判定された場合には、ステップ111に進み、排出ガスセンサ24の異常無し(正常)と判定して、本プログラムを終了する。

#### 【0026】

一方、 $\Delta FAF$ の絶対値と $\Delta\lambda_{tg}$ の絶対値の比が所定範囲から外れていると判定された場合には、ステップ112に進み、排出ガスセンサ24の異常(故障、劣化等)と判定して、運転席のインストルメントパネルに設けられた警告ランプ(図示せず)を点灯し、又は警告表示部(図示せず)に警告表示して運転者に警告すると共に、その異常情報(異常コード)をECU27のバックアップRAM(図示せず)に記憶して、本プログラムを終了する。

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**【0027】**

【気筒間ばらつき検出プログラム】

図3及び図4に示す気筒間ばらつき検出プログラムは、例えば、イグニッションスイッチ(図示せず)のオン後に所定周期で実行され、特許請求の範囲でいう気筒間ばらつき検出手段としての役割を果たす。

**【0028】**

ここで、図5に示すように、吸気管圧力センサ18で検出した吸気管圧力の波形は、各気筒の運転状態(吸入空気量、燃焼状態、空燃比等)を反映した脈動波形となる。従って、各気筒の影響が現れるクランク角範囲毎に吸気管圧力センサ18で検出した吸気管圧力の極小値、極大値、平均値、振幅値、面積、軌跡長等の特性値を算出すれば、各気筒の運転状態を反映した脈動波形の特性値を算出することができるので、この特性値を用いれば、各気筒の運転状態のばらつきを反映した気筒間ばらつき値を算出することができる。

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**【0029】**

尚、本プログラムでは、吸気管圧力の極小値を用いて気筒間ばらつき値を算出するため、図5(a)に示すように、後述する第1～第4のクランク角範囲は、それぞれ第1～第4気筒の影響で吸気管圧力が極小値となる領域を含むように設定されている。

**【0030】**

本プログラムが起動されると、まず、ステップ201で、気筒間ばらつき検出の実行条件が成立しているか否かを、例えば、定常状態(過渡状態ではない)か否か等によって判定する。気筒間ばらつき検出の実行条件が不成立と判定されれば、以降の処理を行うことなく、本プログラムを終了する。

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**【0031】**

一方、上記ステップ201で、気筒間ばらつき検出の実行条件が成立していると判定された場合には、ステップ202に進み、クランク角センサ26の出力信号に基づいて検出したクランク角が第1のクランク角範囲(第1気筒#1の影響で吸気管圧力が極小値となる領域を含むクランク角範囲)内であるか否かを判定する。その結果、第1のクランク角範囲内であると判定されれば、ステップ203に進み、第1のクランク角範囲内における吸気管圧力の極小値P Min を、第1気筒#1の吸気管圧力極小値P Min (#1)として算出する。

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**【0032】**

一方、上記ステップ202で、クランク角が第1のクランク角範囲内ではないと判定された場合には、ステップ204に進み、クランク角が第2のクランク角範囲(第2気筒#2の影響で吸気管圧力が極小値となる領域を含むクランク角範囲)内であるか否かを判定する。その結果、第2のクランク角範囲内であると判定されれば、ステップ205に進み、第2のクランク角範囲内における吸気管圧力の極小値P Min を、第2気筒#2の吸気管圧力極小値P Min (#2)として算出する。

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**【0033】**

また、上記ステップ204で、クランク角が第2のクランク角範囲内ではないと判定された場合には、ステップ206に進み、クランク角が第3のクランク角範囲(第3気筒#3の影響で吸気管圧力が極小値となる領域を含むクランク角範囲)内であるか否かを判定する。その結果、第3のクランク角範囲内であると判定されれば、ステップ207に進み、第3のクランク角範囲内における吸気管圧力の極小値P Min を、第3気筒#3の吸気管圧力極小値P Min (#3)として算出する。

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**【0034】**

また、上記ステップ206で、クランク角が第3のクランク角範囲内ではないと判定された場合には、クランク角が第4のクランク角範囲(第4気筒#4の影響で吸気管圧力が極小値となる領域を含むクランク角範囲)内であると判断して、ステップ208に進み、第4のクランク角範囲内における吸気管圧力の極小値P Min を、第4気筒#4の吸気管圧力極小値P Min (#4)として算出する。

**【0035】**

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この後、図4のステップ209に進み、全気筒の吸気管圧力極小値 $P_{Mm i n}$ (#1)～ $P_{Mm i n}$ (#4)の平均値 $A V E P_{Mm i n}$ を算出する。

$$A V E P_{Mm i n} = \{P_{Mm i n}(#1) + \dots + P_{Mm i n}(#4)\} / 4$$

【0036】

この後、ステップ210に進み、各気筒の吸気管圧力極小値 $P_{Mm i n}$ (#i)と平均値 $A V E P_{Mm i n}$ とを用いて各気筒の気筒間ばらつき値 $D E V$ (#i)を次式により算出する。ここで、#i = #1～#4である。

$$D E V(#i) = P_{Mm i n}(#i) - A V E P_{Mm i n}$$

【0037】

この後、ステップ211に進み、各気筒の気筒間ばらつき値 $D E V$ (#i)が、それぞれ所定範囲内( $K_1 \leq D E V(#i) \leq K_2$ )であるか否かを判定する。その結果、全ての気筒間ばらつき値 $D E V$ (#1)～ $D E V$ (#4)のうち1つでも所定範囲から外れていれば判定された場合には、ステップ212に進み、気筒間ばらつきフラグ $X D E V$ を気筒間ばらつきが大きいことを意味する「1」にセットして、本プログラムを終了する。

【0038】

一方、全ての気筒間ばらつき値 $D E V$ (#1)～ $D E V$ (#4)が所定範囲内であると判定された場合には、ステップ213に進み、気筒間ばらつきフラグ $X D E V$ を気筒間ばらつきが小さいことを意味する「0」にリセットして、本プログラムを終了する。

【0039】

【気筒間ばらつき補正プログラム】

図6に示す気筒間ばらつき補正プログラムは、例えば、イグニッションスイッチのオン後に所定周期で実行され、特許請求の範囲でいう気筒間ばらつき補正手段としての役割を果たす。本プログラムが起動されると、まず、ステップ301で、各気筒の気筒間ばらつき値 $D E V$ (#i)を読み込んだ後、ステップ302に進み、各気筒の気筒間ばらつき値 $D E V$ (#i)を用いて、各気筒の燃料噴射時間補正係数 $F T A U$ (#i)を次式により算出する。

$$F T A U(#i) = D E V(#i) + 1$$

【0040】

この後、ステップ303に進み、補正前の全気筒の平均燃料噴射時間 $T A U$ に各気筒の燃料噴射時間補正係数 $F T A U$ (#i)を乗算して、各気筒の最終燃料噴射時間 $T A U$ (#i)を求める。

$$T A U(#i) = T A U \times F T A U(#i)$$

以上の処理により、各気筒の気筒間ばらつき値 $D E V$ (#i)に応じて各気筒の燃料噴射量を補正することで、気筒間の空燃比ばらつきを小さくする。

【0041】

【誤診断防止プログラム】

図7に示す誤診断防止プログラムは、例えば、イグニッションスイッチのオン後に所定周期で実行され、特許請求の範囲でいう誤診断防止手段としての役割を果たす。本プログラムが起動されると、まず、ステップ401で、▲1▼気筒間ばらつきが小さい(気筒間ばらつきフラグ $X D E V = 0$ )か否かを判定し、また、▲2▼気筒間ばらつき補正が完了してから所定期間(所定時間、所定クランク角等)が経過したか否かを判定する。

【0042】

その結果、気筒間ばらつきが大きい(気筒間ばらつきフラグ $X D E V = 1$ )と判定された場合、又は、気筒間ばらつき補正完了から所定期間が経過する前であると判定された場合には、気筒間ばらつきによって排出ガスセンサ24の出力が乱れて異常診断パラメータ(例えば $\Delta F A F / \Delta \lambda t g$ )が正常範囲( $K C G L \sim K C G H$ )から外れる可能性があると判断して、ステップ402に進み、排出ガスセンサ24の異常診断を禁止する。これにより、気筒間ばらつきによって生じた排出ガスセンサ24の出力の乱れを排出ガスセンサ24の異常と誤診断してしまうことを防止する。

【0043】

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一方、上記ステップ401で、気筒間ばらつきが小さいと判定された場合、又は、気筒間ばらつき補正が完了してから所定期間が経過したと判定された場合には、ステップ403に進み、排出ガスセンサ24の異常診断を許可する。

#### 【0044】

以上説明した本実施形態(1)では、気筒間ばらつきが大きいときに、排出ガスセンサ24の異常診断を禁止するようにしたので、気筒間ばらつきによって生じた排出ガスセンサ24の出力の乱れを排出ガスセンサ24の異常と誤診断してしまうことを防止することができ、排出ガスセンサ24の異常診断精度を向上させることができる。

#### 【0045】

また、本実施形態(1)では、気筒間ばらつき補正を実行してから実際に気筒間ばらつきが十分に小さくなるまでには暫く時間が掛かることがあることを考慮して、気筒間ばらつき補正の完了後も所定期間が経過するまで、排出ガスセンサ24の異常診断の禁止を継続するようにしたので、気筒間ばらつき補正の完了直後で気筒間ばらつきが十分に小さくなっている可能性がある期間にも、異常診断を禁止して、より確実に誤診断を防止することができる。

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#### 【0046】

しかしながら、必ずしも、気筒間ばらつき補正完了から所定期間が経過するまで異常診断の禁止を継続する必要はなく、気筒間ばらつき補正によって速やかに気筒間ばらつきが小さくなるような場合には、気筒間ばらつき補正完了直後に、直ちに排出ガスセンサ24の異常診断を許可するようにしても良い。

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#### 【0047】

##### 《実施形態(2)》

次に、図8乃至図10を用いて本発明の実施形態(2)を説明する。

前記実施形態(1)では、吸気管圧力の極小値を用いて気筒間ばらつき値を算出したが、本実施形態(2)では、後述する図8及び図9に示す気筒間ばらつき検出プログラムを実行することで、吸気管圧力の極大値を用いて気筒間ばらつき値を算出するようにしている。

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#### 【0048】

また、前記実施形態(1)では、誤診断防止のために排出ガスセンサ24の異常診断を禁止するようにしたが、本実施形態(2)では、後述する図10に示す誤診断防止プログラムを実行することで、誤診断防止のために排出ガスセンサ24の異常判定基準を緩和するようにしている。

#### 【0049】

##### [気筒間ばらつき検出プログラム]

図8及び図9に示す気筒間ばらつき検出プログラムでは、吸気管圧力の極大値を用いて気筒間ばらつき値を算出するため、図5(b)に示すように、後述する第1～第4のクランク角範囲は、それぞれ第1～第4気筒の影響で吸気管圧力が極大値となる領域を含むよう設定されている。

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#### 【0050】

本プログラムでは、ステップ501で気筒間ばらつき検出の実行条件が成立していると判定された場合、クランク角が第1のクランク角範囲(第1気筒#1の影響で吸気管圧力が極大値となる領域を含むクランク角範囲)内のときに、該第1のクランク角範囲内における吸気管圧力の極大値P<sub>Mmax</sub>を、第1気筒#1の吸気管圧力極大値P<sub>Mmax</sub>(#1)として算出する(ステップ502、503)。

#### 【0051】

一方、クランク角が第2のクランク角範囲(第2気筒#2の影響で吸気管圧力が極大値となる領域を含むクランク角範囲)内のときに、該第2のクランク角範囲内における吸気管圧力の極大値P<sub>Mmax</sub>を、第2気筒#2の吸気管圧力極大値P<sub>Mmax</sub>(#2)として算出する(ステップ504、505)。

#### 【0052】

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また、クランク角が第3のクランク角範囲（第3気筒#3の影響で吸気管圧力が極大値となる領域を含むクランク角範囲）内のときに、該第3のクランク角範囲内における吸気管圧力の極大値 $P_{Mmax}$ を、第3気筒#3の吸気管圧力極大値 $P_{Mmax}(\#3)$ として算出する（ステップ506、507）。

#### 【0053】

また、クランク角が第4のクランク角範囲（第4気筒#4の影響で吸気管圧力が極大値となる領域を含むクランク角範囲）内のときに、該第4のクランク角範囲内における吸気管圧力の極大値 $P_{Mmax}$ を、第4気筒#4の吸気管圧力極大値 $P_{Mmax}(\#4)$ として算出する（ステップ508）。

#### 【0054】

この後、図9のステップ509に進み、全気筒の吸気管圧力極大値 $P_{Mmax}(\#1) \sim P_{Mmax}(\#4)$ の平均値 $AVEP_{Mmax}$ を算出する。

$$AVEP_{Mmax} = \{P_{Mmax}(\#1) + \dots + P_{Mmax}(\#4)\} / 4$$

#### 【0055】

この後、ステップ510に進み、各気筒の吸気管圧力極大値 $P_{Mmax}(\#i)$ と平均値 $AVEP_{Mmax}$ とを用いて各気筒の気筒間ばらつき値 $DEV(\#i)$ を次式により算出する。

$$DEV(\#i) = P_{Mmax}(\#i) - AVEP_{Mmax}$$

#### 【0056】

この後、ステップ511に進み、各気筒の気筒間ばらつき値 $DEV(\#i)$ が、それぞれ所定範囲（K1～K2）内であるか否かを判定し、全ての気筒間ばらつき値 $DEV(\#1) \sim DEV(\#4)$ のうち1つでも所定範囲を越えていると判定された場合には、ステップ512に進み、気筒間ばらつきフラグ $XDEV$ を「1」にセットし、全ての気筒間ばらつき値 $DEV(\#1) \sim DEV(\#4)$ が所定範囲内であると判定された場合には、ステップ513に進み、気筒間ばらつきフラグ $XDEV$ を「0」にリセットする。

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#### 【0057】

##### 【誤診断防止プログラム】

図10に示す誤診断防止プログラムでは、まず、ステップ601で、▲1▼気筒間ばらつきが小さい（気筒間ばらつきフラグ $XDEV = 0$ ）か否かを判定し、また、▲2▼気筒間ばらつき補正が完了したか否かを判定する。

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#### 【0058】

その結果、気筒間ばらつきが大きい（気筒間ばらつきフラグ $XDEV = 1$ ）と判定された場合、又は、気筒間ばらつき補正が未完了であると判定された場合には、気筒間ばらつきによって排出ガスセンサ24の出力が乱れて異常診断パラメータ（例えば $\Delta FAF / \Delta \lambda_{tg}$ ）が正常範囲（下限値 $KCGL$ ～上限値 $KCGH$ ）から外れる可能性があると判断して、ステップ602に進み、正常範囲の下限値 $KCGL$ （異常判定値）を誤診断防止用の下限値（ $KCGL - \alpha$ ）に変更し、上限値 $KCGH$ （異常判定値）を誤診断防止用の上限値（ $KCGH + \beta$ ）に変更して、正常範囲の幅を広げて異常判定基準を緩和する。これにより、気筒間ばらつきによって生じた排出ガスセンサ24の出力の乱れを排出ガスセンサ24の異常と誤診断することを防止する。

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#### 【0059】

一方、上記ステップ601で、気筒間ばらつきが小さいと判定された場合、又は、気筒間ばらつき補正が完了したと判定された場合には、ステップ603に進み、正常範囲の下限値（異常判定値）と上限値（異常判定値）を通常の値 $KCGL$ 、 $KCGH$ に戻す。

#### 【0060】

以上説明した本実施形態（2）では、気筒間ばらつきが大きいときや気筒間ばらつき補正が未完了のときに、正常範囲の幅を広げて異常判定基準を緩和するようにしたので、気筒間ばらつきによって生じた排出ガスセンサ24の出力の乱れを排出ガスセンサ24の異常と誤診断してしまうことを防止することができ、排出ガスセンサ24の異常診断精度を向上させることができる。

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**【0061】**

尚、本実施形態（2）では、異常判定基準を緩和するために異常判定値（正常範囲の下限値と上限値）を変更するようにしたが、異常診断パラメータ（例えば $\Delta F A F / \Delta \lambda t g$ ）を補正したり、排出ガスセンサ24の出力を補正する等、他の異常判定条件を変更するようにも良い。

**【0062】**

また、本実施形態（2）においても、前記実施形態（1）と同じように、気筒間ばらつき補正完了後も所定期間が経過するまで、異常判定基準の緩和を継続するようにしても良い。

**【0063】**

また、上記各実施形態（1），（2）では、本発明を排出ガスセンサ24の異常診断に適用したが、本発明はこれに限定されず、例えば、排出ガスセンサ24の出力を用いた触媒劣化診断、エアフローメータ14の出力を用いたエアフローメータ14の異常診断、吸気管圧力センサ18の出力を用いた吸気管圧力センサ18の異常診断、エアフローメータ14と吸気管圧力センサ18と排出ガスセンサ24のうちの少なくとも1つの出力を用いた触媒早期暖機システムの異常診断や空燃比制御システムの異常診断等、気筒間ばらつきの影響を受ける種々の異常診断に本発明を適用することができる。10

**【0064】**

また、上記各実施形態（1），（2）では、吸気管圧力の所定期間毎の極大値又は極小値に基づいて気筒間ばらつき値を算出したが、気筒間ばらつき値の算出方法は適宜変更しても良く、例えば、吸気管圧力の所定期間毎の平均値、振幅値、面積、軌跡長等に基づいて気筒間ばらつき値を算出するようにしても良い。また、吸気管圧力に代えて、吸入空気量、筒内圧力、回転速度、イオン電流、空燃比等に基づいて気筒間ばらつき値を算出するようにも良い。20

**【0065】**

また、上記各実施形態（1），（2）では、各気筒毎に燃料噴射量を補正することで気筒間ばらつきを補正したが、気筒間ばらつきの補正方法は適宜変更しても良く、例えば、各気筒毎に点火時期を補正したり、各気筒毎に吸入空気量を補正して気筒間ばらつきを補正するようにしても良い。

**【0066】**

その他、本発明の適用範囲は4気筒のエンジンに限定されず、5気筒以上又は3気筒以下の複数気筒エンジンに本発明を適用しても良い。30

**【図面の簡単な説明】**

**【図1】**本発明の実施形態（1）におけるエンジン制御システム全体の概略構成図

**【図2】**実施形態（1）の排出ガスセンサ異常診断プログラムの処理の流れを示すフローチャート

**【図3】**実施形態（1）の気筒間ばらつき検出プログラムの処理の流れを示すフローチャート（その1）

**【図4】**実施形態（1）の気筒間ばらつき検出プログラムの処理の流れを示すフローチャート（その2）

**【図5】**吸気管圧力の挙動を示すタイムチャート

**【図6】**実施形態（1）の気筒間ばらつき補正プログラムの処理の流れを示すフローチャート

**【図7】**実施形態（1）の誤診断防止プログラムの処理の流れを示すフローチャート

**【図8】**実施形態（2）の気筒間ばらつき検出プログラムの処理の流れを示すフローチャート（その1）

**【図9】**実施形態（2）の気筒間ばらつき検出プログラムの処理の流れを示すフローチャート（その2）

**【図10】**実施形態（2）の誤診断防止プログラムの処理の流れを示すフローチャート

**【符号の説明】**

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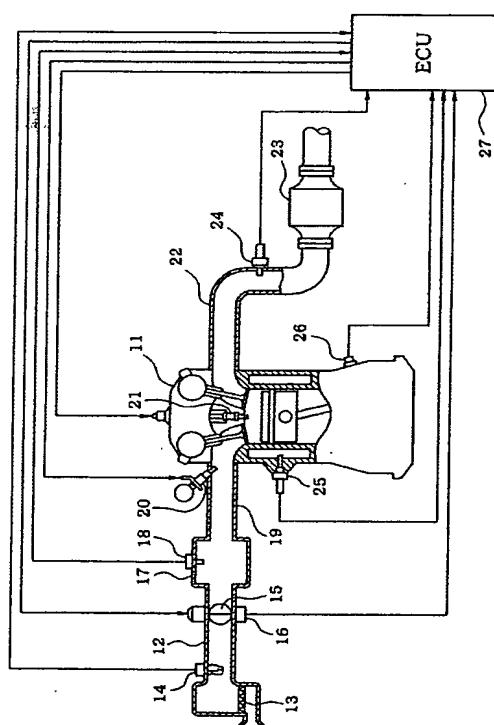
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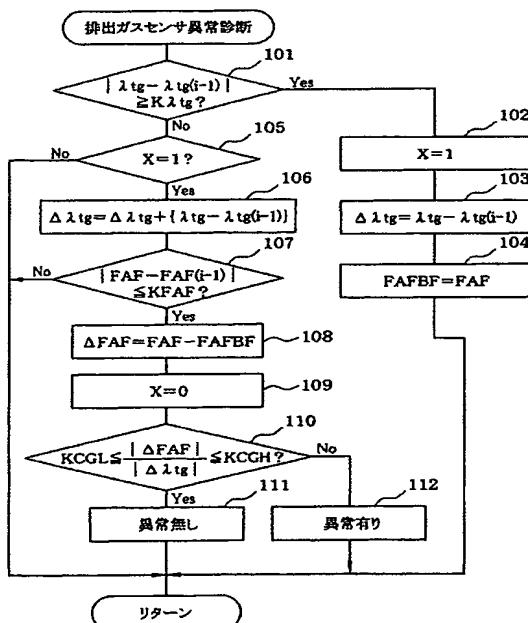
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11…エンジン（内燃機関）、12…吸気管、14…エアフローメータ、15…スロットルバルブ、18…吸気管圧力センサ、20…燃料噴射弁、21…点火プラグ、22…排気管、24…排出ガスセンサ、26…クランク角センサ、27…ECU（異常診断手段、気筒間ばらつき検出手段、気筒間ばらつき補正手段、誤診断防止手段）。

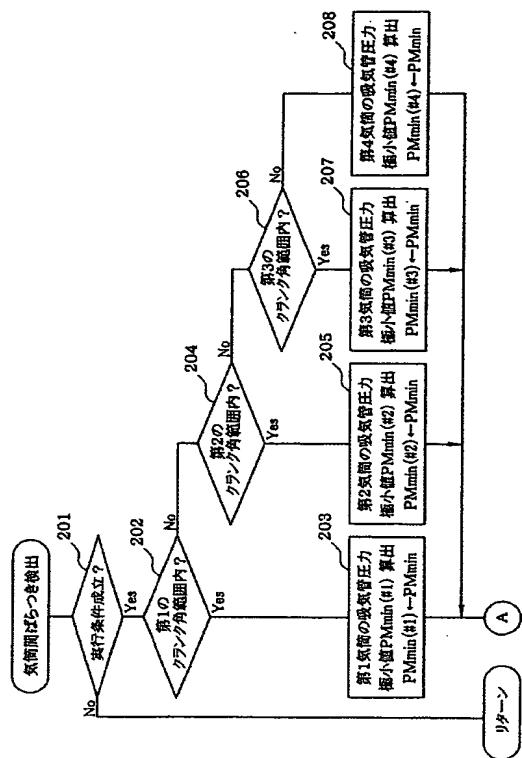
【図1】



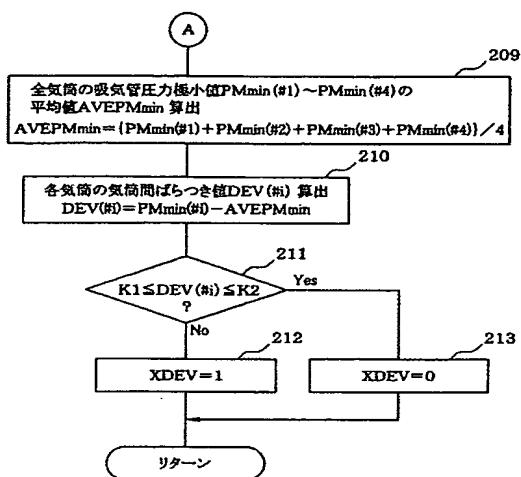
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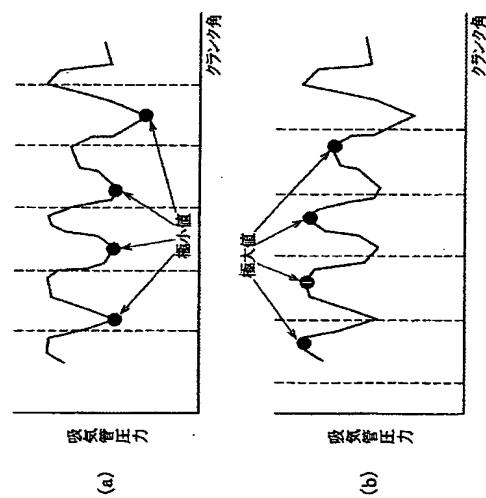
【図3】



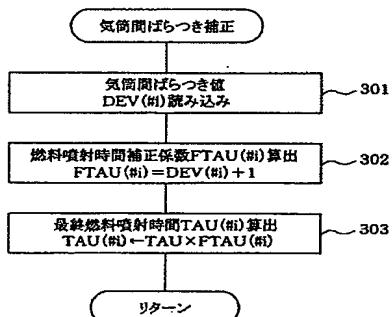
【図4】



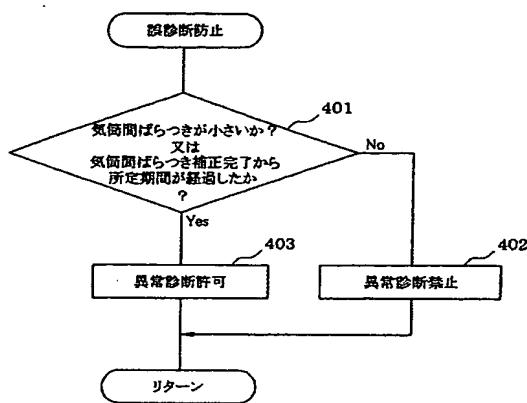
【図5】



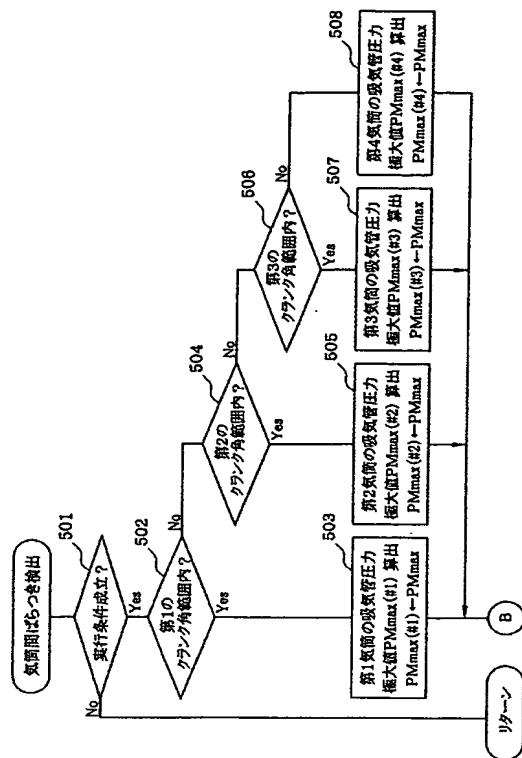
【図6】



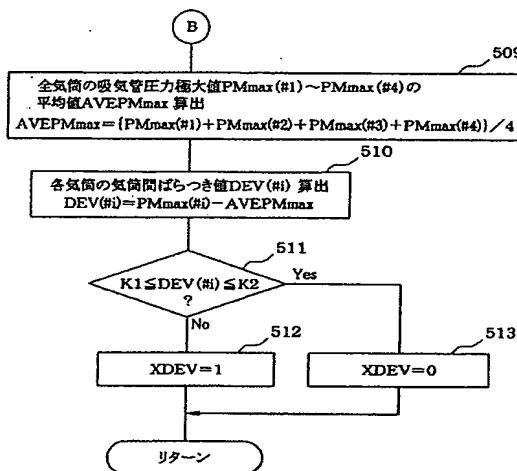
【図 7】



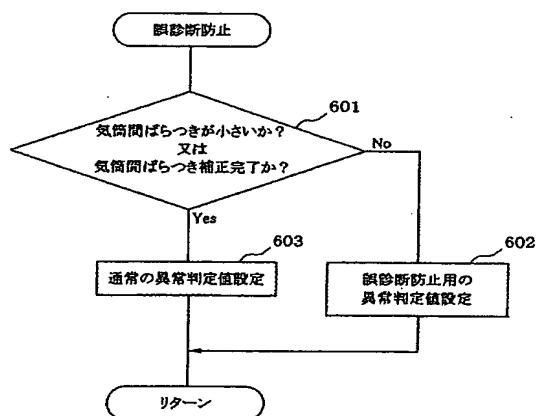
【図 8】



【図 9】



【図 10】



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フロントページの続き

F ターム(参考) 3G301 HA01 JA05 JB09 JB10 LA03 NA08 NC01 ND05 NE17 NE23  
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